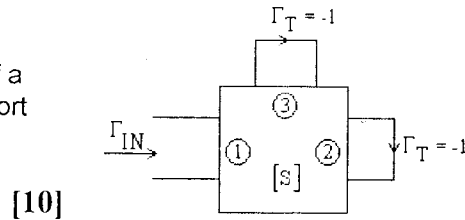


All symbols and variables have their usual meaning.

Note 1: The numbers in square brackets at the right-hand side of the text indicate the provisional allocation of maximum marks per question or sub-section of a question.

Q.1 Calculate the input reflection coefficient (at port 1) of a three port network where ports 2 and 3 are terminated by short circuits.



[10]

Q.2 Design an amplifier for maximum gain at 5.0 GHz with a GaAs FET that has the following S parameters ($Z_0=50\Omega$):

$$[S] = \begin{bmatrix} 0.65\angle -140^\circ & 0.04\angle 60^\circ \\ 2.4\angle 50^\circ & 0.70\angle -65^\circ \end{bmatrix}$$

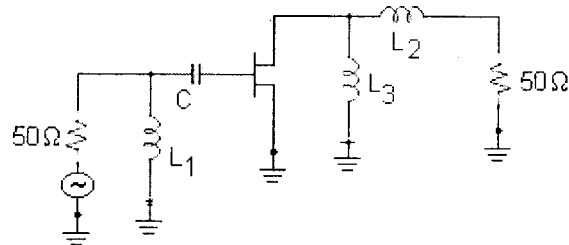
Design matching sections using open-circuited shunt stubs.

[10]

Q.3 Design an amplifier with maximum G_{TU} using a transistor with the following S parameters ($Z_0=50\Omega$) at 6.0 GHz:

$$[S] = \begin{bmatrix} 0.61\angle -170^\circ & 0.0 \\ 2.24\angle 32^\circ & 0.72\angle -83^\circ \end{bmatrix}$$

Design L-section matching sections using lumped elements as shown in the fig.



[10]

Q.4 A GaAs FET has the following scattering and noise parameters at 6.0 GHz ($Z_0=50\Omega$):

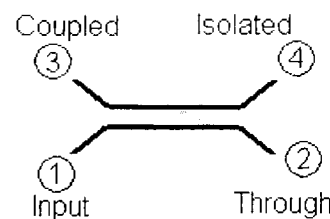
$$[S] = \begin{bmatrix} 0.6\angle -60^\circ & 0.0 \\ 2.0\angle 81^\circ & 0.7\angle -60^\circ \end{bmatrix} \text{ and } .$$

$F_{MIN}=2.0$ dB, $\Gamma_{opt} = 0.62\angle 100^\circ$, and $R_N=20\Omega$. Design an amplifier to have a gain of 6 dB, and the minimum noise figure possible with this gain. Design matching sections using open-circuited shunt stubs.

[10]

Q.5 A directional coupler has the scattering matrix given below. Find the directivity, coupling, insertion loss, and the return loss at the input port when the other ports are terminated in matched loads.

$$[S] = \begin{bmatrix} 0.032\angle 30^\circ & 0.96\angle 0^\circ & 0.1\angle 90^\circ & 0.0018\angle 90^\circ \\ 0.96\angle 0^\circ & 0.032\angle 30^\circ & 0.0018\angle 90^\circ & 0.1\angle 90^\circ \\ 0.1\angle 90^\circ & 0.0018\angle 90^\circ & 0.034\angle 30^\circ & 0.018\angle 0^\circ \\ 0.0018\angle 90^\circ & 0.1\angle 90^\circ & 0.018\angle 0^\circ & 0.033\angle 30^\circ \end{bmatrix}$$



[10]

Contd.

Note 2:

You may need:

$$T = \frac{P_1(1 - \Sigma L_1^1 + \Sigma L_2^1 + \dots) + P_2(1 - \Sigma L_1^2 + \Sigma L_2^2 + \dots) + \dots}{1 - \Sigma L_1 + \Sigma L_2 + \dots}$$

$$\mu = \frac{1 - |S_{11}|^2}{|S_{22} - \Delta S_{11}^*| + |S_{12} S_{21}|}; \quad K = \frac{1 - |S_{11}|^2 - |S_{22}|^2 + |\Delta|^2}{2|S_{12} S_{21}|};$$

$$B_1 = 1 + |S_{11}|^2 - |S_{22}|^2 - |\Delta|^2; \quad B_2 = 1 - |S_{11}|^2 + |S_{22}|^2 - |\Delta|^2; \quad C_1 = S_{11} - \Delta S_{22}^*; \quad C_2 = S_{22} - \Delta S_{11}^*;$$

$$\Gamma_{ML} = \frac{B_2 - \sqrt{B_2^2 - 4|C_2|^2}}{2C_2}; \quad \Gamma_{MS} = \frac{B_1 - \sqrt{B_1^2 - 4|C_1|^2}}{2C_1}; \quad G_{TM} = \frac{|S_{21}|}{|S_{12}|} (K - \sqrt{K^2 - 1});$$

$$G_T = \frac{1 - |\Gamma_s|^2}{|1 - \Gamma_{IN} \Gamma_s|^2} |S_{21}|^2 \frac{1 - |\Gamma_L|^2}{|1 - S_{22} \Gamma_L|^2}; \quad G_{TU} = \frac{1 - |\Gamma_s|^2}{|1 - S_{11} \Gamma_s|^2} |S_{21}|^2 \frac{1 - |\Gamma_L|^2}{|1 - S_{22} \Gamma_L|^2} = G_{IU} G_0 G_{2U}$$

$$U = \frac{|S_{11} S_{22} S_{12} S_{21}|}{(1 - |S_{11}|^2)(1 - |S_{22}|^2)}; \quad \frac{1}{(1+U)^2} < \frac{G_T}{G_{TU}} < \frac{1}{(1-U)^2}$$

$$g_i = \frac{G_{IU}}{G_{i\max}} = G_{IU} (1 - |S_{ii}|^2); \quad d_i = \frac{g_i |S_{ii}|}{1 - |S_{ii}|^2 (1 - g_i)}; \quad R_i = \frac{\sqrt{1 - g_i} (1 - |S_{ii}|^2)}{1 - |S_{ii}|^2 (1 - g_i)};$$

$$C_S = \frac{(S_{11} - \Delta S_{22}^*)^*}{|S_{11}|^2 - |\Delta|^2}; \quad R_S = \frac{|S_{12} S_{21}|}{||S_{11}|^2 - |\Delta|^2|}; \quad C_L = \frac{(S_{22} - \Delta S_{11}^*)^*}{|S_{22}|^2 - |\Delta|^2}; \quad R_L = \frac{|S_{12} S_{21}|}{||S_{22}|^2 - |\Delta|^2|}$$

$$G_p = |S_{21}|^2 g_p; \quad g_p = \frac{1 - |\Gamma_L|^2}{|1 - S_{22} \Gamma_L|^2 - |S_{11} - \Delta \Gamma_L|^2};$$

$$g_p = \frac{1 - |\Gamma_L|^2}{1 - |S_{11}|^2 + |\Gamma_L|^2 (|S_{22}|^2 - |\Delta|^2) - 2 \operatorname{Re}(\Gamma_L C_2)};$$

$$G_A = |S_{21}|^2 g_A; \quad g_A = \frac{1 - |\Gamma_s|^2}{|1 - S_{11} \Gamma_s|^2 - |S_{22} - \Delta \Gamma_s|^2};$$

$$g_A = \frac{1 - |\Gamma_s|^2}{1 - |S_{22}|^2 + |\Gamma_s|^2 (|S_{11}|^2 - |\Delta|^2) - 2 \operatorname{Re}(\Gamma_s C_1)};$$

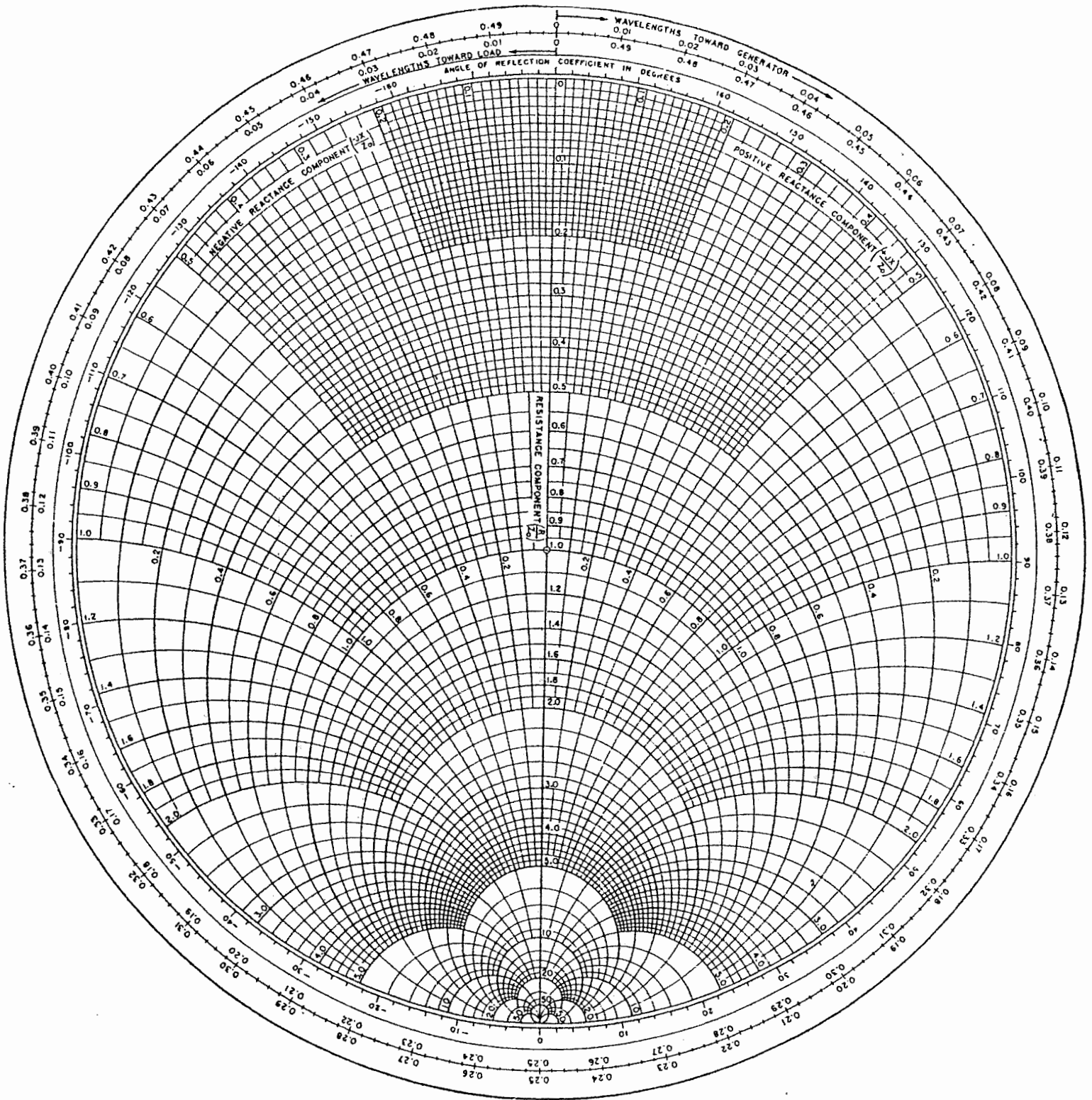
$$R_p = \frac{[1 - 2K |S_{12} S_{21}| g_p + |S_{12} S_{21}|^2 g_p^2]^{1/2}}{|1 + g_p (|S_{22}|^2 - |\Delta|^2)|}; \quad C_p = \frac{g_p C_2^*}{1 + g_p (|S_{22}|^2 - |\Delta|^2)};$$

$$F = F_1 + \frac{F_2 - 1}{G_1}; \quad F = F_{MIN} + \frac{R_N}{G_S} |Y_S - Y_{OPT}|^2; \quad Y_S = \frac{1}{Z_0} \frac{1 - \Gamma_s}{1 + \Gamma_s}; \quad Y_{OPT} = \frac{1}{Z_0} \frac{1 - \Gamma_{OPT}}{1 + \Gamma_{OPT}};$$

$$C_F = \frac{\Gamma_{OPT}}{N+1}; \quad R_F = \frac{\sqrt{N(N+1 - |\Gamma_{OPT}|^2)}}{N+1}; \quad \text{where } N = \frac{|\Gamma_s - \Gamma_{OPT}|^2}{1 - |\Gamma_s|^2} = \frac{F - F_{MIN}}{4R_N / Z_0} |1 + \Gamma_{OPT}|^2$$

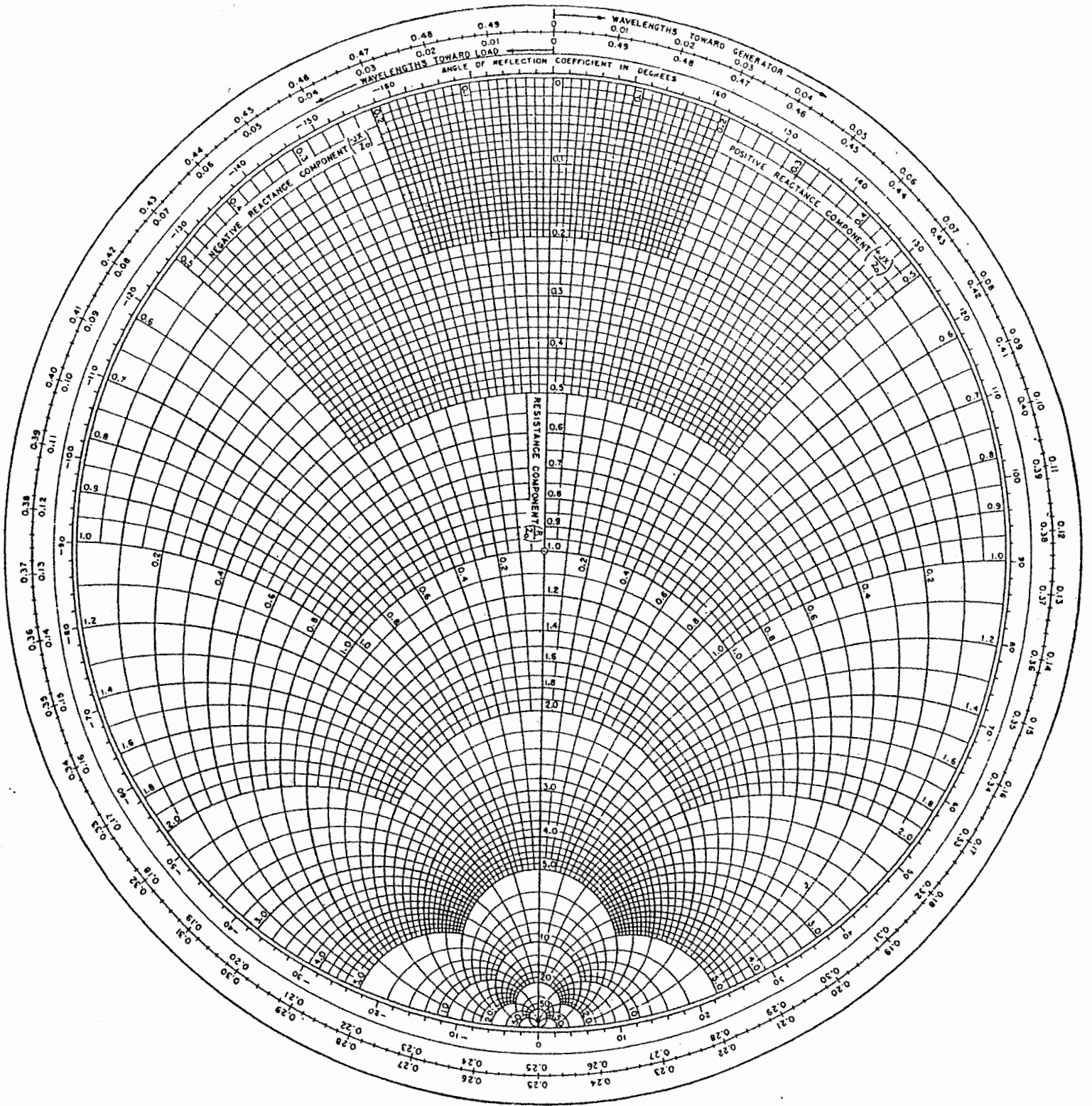
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